Geologic mapping as a tool for predicting groundwater contamination: Assessing arsenic risk in east-central Wisconsin

> Eric Stewart Billy Fitzpatrick





## Acknowledgements

• Synthesizing ideas and work from many people



Sarah Bremmer– Grant County geologic mapping



Billy Fitzpatrick – Geochemistry



Ken Bradbury – Hydraulic conductivity estimates



Steve Mauel – GIS and regional geology



Bill Batten – Fond du Lac county map



Esther Stewart – Dodge County geologic map

## Purpose

• Dissolved arsenic in groundwater wells is a longstanding problem in eastern Wisconsin

- 48.5% of wells reported by the WDNR in Fond du Lac and Dodge counties detected As over 2 ug/L
- Can we use geologic mapping to better understand and predict areas of elevated risk?

Focus area



Dissolved arsenic in groundwater wells



## Overview

- Mapping Paleozoic rocks of Wisconsin
- How do folds and faults alter bedrock units?
- Stratigraphic and well construction controls on arsenic in wells
- What matters to communities?
  - GRAC project investigating a link between groundwater contamination and folding
- Summary What we've learned



## Location and Age of Paleozoic rocks in Wisconsin







Mountain Press 2004



## Mapping approach today



- Depends on the location and scale
  - In Driftless area at 1:24,000 scale, field work





Stewart and others (in revision)

## Approach today

 At 1:100,000 and in glaciated parts of the state, we create 3D surfaces of unit contacts, and intercept them with a bedrock surface





# Map is made by intersecting contact surfaces with a bedrock surface

 Create 3D surfaces of unit contacts, and intercept them with a bedrock surface





# Map is made by intersecting contact surfaces with a bedrock surface

 Create 3D surfaces of unit contacts, and intercept them with a bedrock surface









Wisconsin Geological Natural History Survey Division of extension Niversity of Wisconsin-Madison

Fold axes based on folding of underlying base Prairie du Chien surface

## What are they?

• In many cases, folds form when Precambrian basement was reactivated in the Paleozoic



## Paleozoic folds in Wisconsin are subtle

#### • Mineral Point anticline – near Fennimore, Grant County, SW Wisconsin



10 times vertically exaggerated

#### Cross section from Bremmer and others (in prep)





## Small fault-propagation fold involving Precambrian basement



Cross section from Bremmer and others (in prep), vertical exaggeration 10 times

• Some Paleozoic folds may be cut by faults, in others, the faults may be buried



Finch and others (2003)

## Small fault-propagation folds



Cross section from Bremmer and others (in prep)

 Some Paleozoic folds may be cut by faults, in others, the faults may be buried





### Paleozoic folds in Wisconsin are subtle





10 times vertically exaggerated

## Overview

- Mapping Paleozoic rocks of Wisconsin
- How do folds and faults alter bedrock units
- Stratigraphic and well construction controls on arsenic in wells
- What matters to communities?
  - GRAC project investigating a link between groundwater contamination and folding
- Summary What we've learned
  - Map scale and approach



## Southwest Wisconsin: Increased fracturing observed near faults



Heavily fractured Galena Formation, faulted zone along Mineral Point anticline





10 times vertically exaggerated

## Deformation bands

Reduction in sandstone porosity in deformation bands may lead to reduction in horizontal hydraulic conductivity









# Fracturing in bedrock units in glaciated parts of the state







Structure contour map based on mapping by Batten (2018) and Stewart (2021)

## Regional geology

 Folds probably formed from reactivated
 Precambrian structures







Base map from aeromag compilation by E. Anderson, USGS, modified from Daniels and Snyder (2002)



## Fracturing in core in Dodge County

• More fractures/foot near folds than far away



Fond du Lac County Dodge County

Stewart and others (2021)

★ Core location

### Testing the field and core observations with well data



Till, outwash

lacustrine

Dolostone

Sandstone Shale, siltstone sandstone

Sandy

dolostone Calcareous sandstone

Shale

• Estimated hydraulic conductivity (K) from specific capacity tests in wells (Bradbury and Rothschild, 1985)

Property 1 1S PLACE		Tel	lephone	-	_	1. Well Location	Depth 1	72 FT
Owner Mailing		Nu	mber		-	T=Town C=City V=Village	Fire#	
Address W9704 CTY TRK D	0					1 of CALAMUS		
City BEAVER DAM	1W1		ip Code	53	916	W9704 CTY HWY D	1	
County of Well Location	Co Well Permit No	W	ell Con	npletion Da	ite	Subdivision Name Lot#	Block #	Ŧ
14 DODGE	N		09/2	20/199	95			
SAMS ROTARY DRILLER	S INC370	114	4030	0510		Gov't Lot or NE	1/4 of NE	1/4 of
Address		Public	Well P	lan Approv	al#	Section 12 T11 N R	13 E	
City St	te Zip Code	Date	Of ADDD	oval		2. Well Type o (See, item	12 below) 43	26.46
RANDOLPH WI	53956					1=New 2=Replacement 3=Record	struction 88	53.07
Hicap Permanent Well# Con	imon Well #	Specif	ic Capa	city epm/ft		of previous unique well # c	onstructed in 0	_
Well Server # of homes and or B	NP	.0	<u>,</u>	gpurn Wiek Coose		Reason for replaced or reconstructed We	11?	
N (eg: barn, restaurant	, church, school, in	dustry, d	etc.)	Well?	N	BAR		
M-Munic O-OTM N-NonComP-Prints Z-Other X-	NonPot A-Anode L-Lo	op H=Dri	ilhole 1	Property?	Ν	1 1=Drilled 2=Driven Point 3=Jetted 4	-Other	
<ol> <li>Is the well located upslope or sideslope an Well located in floodplain? NI</li> </ol>	d not downslope fro	om any	contami	ination sour	ces, includi	ng those on neighboring properties? Y		
Distance in feet from well to nearest: (includi	ng proposed)	5	<ol> <li>Dow</li> <li>Priv</li> </ol>	nspour Ya W	ru riyaraht	17. Wastew 18. David 4	ater Sump nimal Barn Pen	
1. Landfill 10 2. Puilding Ouerbarry		1	11. Fou	ndation Dra	ain to Cleary	water 19. Animal	Yard or Shelter	
99 3. 1=Septic 2= Holding	Tank	12. Foundation Drain to Sewer			ain to Sewer	20. Silo		
121 4. Sewage Absorption Unit		1	3. Buil	Iding Drain 1=Cast In	on or Plastic	21. Barn Gu	itter	
5. Nonconforming Pit		1	14. Buil	Iding Sewe	r 1=Grav	ity 2=Pressure 22. Manure	Pipe 1=Gravity Cast iron or Plastic	2=Pressure 2=Other
<ol> <li>Buried Home Heating Oil</li> </ol>	Tank	1	15. Coll	1=Ca lector Sewe	ist Iron or P r: units	in diam. 24 Ditch	anure Storage	
<ol> <li>Buried Petroleum Tank</li> <li>1-Shoralina 2- Swime</li> </ol>	ning Pool	1	16. Clea	arwater Sur		25. Other N	R 812 Waste Sourc	e
Drillhole Dimensions and Construction	Mathod							
From To Upper Enl	arged Drillhole	Low	er Open	Bedrock	Geor. Co	de Geol Descrip.	From (ft)	10 (π)
8 0 126 -2. Rotary	<ul> <li>Air</li> </ul>				G	GRAVEL	4	11
surface 3. Rotary	- Air and Foam					LIMEROCK	11	40
6 126 172 -5. Rever	nrougn Casing Ha se Rotary	mmer			N_	SANDROCK	40	172
6. Cable-	tool Bit in. d	dia		- -				
7. Temp. Remo	outer Casing . ved ?	in. di	18	_ depth II.				
Other								
6. Casing Liner Screen Material, Weight,	specification	Fr	om	To (ft)				
C STD BLK PIPE 280 WALL WELD	D JOINTS A53	ourfe		126	1			
SAWHILL		Suit	~	120				
					<ol> <li>Static V</li> <li>30 1</li> </ol>	Vater Level 11.	Well Is: 18 in.	A Grade
		1			10 Burr	A=Above B=Below Dev	eloped? Y	A=Above B=Below
Dia.(in.) Screen type, material &	slot size	Fro	m	То	Pumping	g level 63 ft. below surface Disi	nfected? Y	
		1			Pumpir	ng at 20 GPM 1 Hrs Cap	ped? Y	
				#	<ol> <li>Did yo unused we</li> </ol>	ou notify the owner of the need to permane lls on this property?	ntly abandon and fi	ll all
7. Grout or Other Sealing Material			To	Sacks	If no, exp	blain		
7. Grout or Other Sealing Material Method TREMIE PUMPED		(ft)	(0)	Coment				
7. Grout or Other Sealing Material Method TREMIE PUMPED Kind of Sealing Material		(ft.)	(ft.)	Cement	13. Initials	of Well Constructor or Supervisory Drille	r Date 5 09/2	signed 7/1995
7. Grout or Other Sealing Material Method TREMIE PUMPED Kind of Sealing Material GROUT		from (ft.)	(ff.) 126	Cement	13. Initials Initials of	of Well Constructor or Supervisory Drille JV Drill Rig Operator (Mandatory unless sam	r Date 5 09/2 re as above) Date 5	signed 7/1995 Signed

Hydraulic conductivity (K) = measure of how easily water moves through rock

### Testing the field and core observations with well data

- Estimated hydraulic conductivity (K) from specific capacity tests in wells (Bradbury and Rothschild, 1985)
- High K values in the St. Peter Formation tend to concentrate near mapped structures, suggesting they may be areas of increased fracturing and groundwater flow



and Natural History Survey Division of extension UNIVERSITY OF WISCONSIN-MADISON

Stewart and others (2021)

## Fracturing in core in Dodge County

- Mississippi Valley type sulfide mineralization common in Paleozoic section
- Iron sulfides contain arsenic impurities that can lead to well contamination



Near mapped folds, fracture density is higher and sulfides often fill vertical fractures





 From from folds/faults, little sulfide below the St. Peter Formation





 Near the Beaver Dam anticline, sulfides are more abundant than other cores, and present throughout the stratigraphic section. Dodge County

Highlighted stars = core locations



★ Core location

### Sulfide mineralization

BSE image



Wisconsin Geological and Natural History Surve Division of Extension UNIVERSITY OF WISCONSIN-MADISON Marcasite-rich bands and cement (light gray)



Cataclastic deformation bands with marcasite fill



★ Core location



15.0kV x32 BSECOMP



## Groundwater data compilation – high, moderate and low arsenic values focused near mapped structures



Stewart and others (2021)



#### EPA limit is 10 µg/L



This map only shows groundwater wells with high arsenic values (>100µg/L)

# Conceptual model – role of folds on hydraulic conductivity and arsenic detection

Higher fracture density near folds leads to more sulfide mineralization and/or a deeper oxidation front – perhaps higher arsenic risk for groundwater wells



Stewart and others (2021)



## Overview

- Folds and faults in Paleozoic rocks of Wisconsin
  - They are very small -how do we find them and how do they form?
- How do folds and faults alter bedrock units?
- Stratigraphic and well construction controls on arsenic in wells
- What matters to communities?
  - GRAC project investigating a link between groundwater contamination and folding
- Summary What we've learned



## Other causes of arsenic in groundwater wells



#### Stratigraphic control

## Stratigraphic sources leading to elevated arsenic?

 Sulfide cement horizon (SCH) is a major source of high arsenic concentrations in Winnebago and Outagamie counties



#### Role of stratigraphy - Schreiber et al. 2000



## What about stratigraphic sources and well construction characteristics?

 Sulfide cement horizon (SCH) is a major source of high arsenic concentrations in Winnebago and Outagamie counties



#### Role of stratigraphy - Schreiber et al. 2000



## Far from folds and faults, sulfides are focused in the St. Peter sandstone, particularly at the contact with the overlying Sinnipee Group



#### Typical iron sulfide grain composition (electron microprobe data)



## Despite the abundance of iron sulfide, little arsenic low in section

Sulfide vein and sulfide cemented sandstone

- 57% SiO2
- 17.4 wt% Fe
- < 5 ppm arsenic
- 18 wt% S



## Whole-rock geochemistry

## Sulfide vein and sulfide cemented sandstone

- 63.2 wt% SiO2
- 13.15 wt% Fe
- < 5 ppm arsenic
- 12.35 wt% S



Other well construction characteristics leading to increased arsenic potential in wells – Fe-(hydr)oxides present near bedrock surface

- Sulfides can be oxidized, particularly near the bedrock surface (near atmosphere)
- Fe-(hydr)oxides strongly adsorb dissolved As
- If Fe-(hydr)oxides become unstable in the well borehole, they can release As into well water (e.g. Gotkowitz et al., 2004)



Oxidized sulfide vein



### Whole-rock composition

Wells not cased far below the bedrock surface may be more prone to arsenic problems

#### Oxide-cemented sandstone

- 95.6% SiO2
- 1.61 Fe2O3
- 4.5 ppm arsenic

#### Oxide-cemented sandstone

- 95.4% SiO2
- 2.52 Fe2O3
- 4.7 ppm arsenic







## Oxidized sulfide concretion in sandstone

- 75.5 wt% SiO2
- 19.05 wt% Fe2O3
- 155 ppm arsenic
- 0.03 wt% S

# What about stratigraphic sources for low and moderate arsenic concentrations?

Geographic divide in counties – arsenic problems more common in west

EPA limit = 10 ug/L





## Overview

- Folds and faults in Paleozoic rocks of Wisconsin
  - They are very small -how do we find them and how do they form?
- How do folds and faults alter bedrock units?
- Stratigraphic and well construction controls on arsenic in wells
- What matters to communities?
  - GRAC project investigating a link between groundwater contamination and folding
- Summary What we've learned



# Need some sort of test to determine significance of observations

- Lots of variables might be contributing (folds/faults, sulfide cement horizon, casing versus static water level, casing versus bedrock surface, stratigraphic unit), how do we know relative importance of each?
- Start with Google



## Logistic regression

Test the importance of folds and other variables using logistic regression, a tool that assesses whether a variable(s) changes the probability of an event occurring

Yes event  $\ge x \mu g/L$  dissolved As (where x = 2, 5 or 10  $\mu g/L$ ) No event < x  $\mu g/L$  dissolved As

Tested variables include geologic units, distance to nearest mapped fold, and different well construction parameters





#### **Bold values are statistically significant results**

Table 1         Final model (95% confidence intervals in parentheses)							
		2 μg/L cutoff (n=283)		5 μg/L cutoff (n=283)		10 μg/L cutoff (n=228)	
Variable	Variable Type	Variable (b <sub>i</sub> ) coefficient (multivariate)	Odds ratio	Variable (b <sub>i</sub> ) coefficient (multivariate)	Odds ratio	Variable (b <sub>i</sub> ) coefficient (multivariate)	Odds ratio
Intercept	N/A	<b>0.8398</b> (0.3556, 1.4274)	N/A	<b>-0.3082</b> (-0.8791, 0.2581)	N/A	<b>-0.3126</b> (-0.8671, 0.3436)	N/A
Distance to nearest fold axis	Continuous	<b>-0.3454</b> (-0.5215, -0.2254)	0.7079 (0.5936, 0.7982)	<b>-0.2553</b> (-0.4276, -0.1226)	0.7747 (0.6521, 0.8846)	<b>-0.2689</b> (-0.5821, -0.0900)	0.7642 (0.5587, 0.9139)
Well open to St. Peter Formation	Categorical	<b>0.6532</b> (0.1197, 1.2225)	1.9216 (1.1271, 3.3956)	<b>0.6805</b> (0.1910, 1.2400	1.9748 (1.2104, 3.4555)	N/A	N/A
Well open to units below St. Peter	Categorical	N/A	N/A	N/A	N/A	<b>-1.0684</b> (-2.9185, -0.1396)	0.3436 (0.0540, 0.8697)
Casing depth minus depth to bedrock	Continuous	<b>-0.0056</b> (-0.0092, -0.0026)	0.9945 (0.9908, 0.9974)	<b>-0.0058</b> (-0.0108, -0.0025)	0.9942 (0.9892, 0.9975)	N/A	N/A
Casing depth minus depth to static water level	Continuous	N/A	N/A	N/A	N/A	<b>-0.0125</b> (-0.0245, -0.0008)	0.9876 (0.9758, 0.9992)



#### **Bold values are statistically significant results**

	Table 1         Final model (95% confidence intervals in parentheses)						
		2 μg/L cuto	ff (n=283)	5 μg/L cuto	ff (n=283)	10 μg/L cutoff (n=228)	
Variable	Variable Type	Variable (b <sub>i</sub> ) coefficient (multivariate)	Odds ratio	Variable (b <sub>i</sub> ) coefficient (multivariate)	Odds ratio	Variable (b <sub>i</sub> ) coefficient (multivariate)	Odds ratio
Intercept	N/A	<b>0.8398</b> (0.3556, 1.4274)	N/A	-0.3082 (-0.8791, 0.2581)	N/A	- <b>0.3126</b> (-0.8671, 0.3436)	N/A
	Continuous	- <b>0.3454</b> (-0.5215, -0.2254)	0.7079 (0.5936, 0.7982)	- <b>0.2553</b> (-0.4276, -0.1226)	0.7747 (0.6521, 0.8846)	- <b>0.2689</b> (-0.5821, -0.0900)	0.7642 (0.5587, 0.9139)
Well open to St.		0.6522	1 0 2 1 6	0.6905	1 0749		
Peter Formation	Categorical	(0.1197, 1.2225)	(1.1271, 3.3956)	(0.1910, 1.2400	(1.2104, 3.4555)	N/A	N/A
Well open to units below St. Peter	Categorical	N/A	N/A	N/A	N/A	<b>-1.0684</b> (-2.9185, -0.1396)	0.3436 (0.0540, 0.8697)
Casing depth minus depth to bedrock	Continuous	<b>-0.0056</b> (-0.0092, -0.0026)	0.9945 (0.9908, 0.9974)	<b>-0.0058</b> (-0.0108, -0.0025)	0.9942 (0.9892, 0.9975)	N/A	N/A
Casing depth minus depth to static water level	Continuous	N/A	N/A	N/A	N/A	<b>-0.0125</b> (-0.0245, -0.0008)	0.9876 (0.9758, 0.9992)

Distance to nearest fold/fault significant at cutoffs of 2, 5 and 10



#### **Bold values are statistically significant results**

Table 1 Final model (95% confidence intervals in parentheses) 2 µg/L cutoff (n=283) 5 µg/L cutoff (n=283) 10 µg/L cutoff (n=228) Variable (b<sub>i</sub>) Variable (b<sub>i</sub>) coefficient Variable (b<sub>i</sub>) coefficient coefficient Odds ratio Odds ratio Variable Type Odds ratio (multivariate) (multivariate) (multivariate) 0.8398 -0.3082 -0.3126 N/A N/A N/A N/A Intercept (0.3556, 1.4274)(-0.8791, 0.2581)(-0.8671, 0.3436)Distance to -0.3454 0.7079 -0.2553 0.7747 -0.2689 0.7642 Continuous (-0.5215, -0.2254) <del>(0.5936, 0.7982)</del> (-0.4276, -0.1226)(0.6521, 0.8846)(-0.5821, -0.0900)(0.5587, 0.9139)0.6532 1.9216 0.6805 1.9748 Categorical N/A N/A (0.1197, 1.2225)(1.1271, 3.3956)(0.1910, 1.2400)(1.2104, 3.4555)-1.0684 0.3436 Categorical N/A N/A N/A N/A (-2.9185, -0.1396)(0.0540, 0.8697)-0.0056 0.9945 -0.0058 0.9942 minus depth to Continuous N/A N/A (-0.0092, -0.0026)(0.9908, 0.9974)(-0.0108, -0.0025)(0.9892, 0.9975)Casing depth 0.9876 -0.0125 minus depth to Continuous N/A N/A N/A N/A (-0.0245, -0.0008)(0.9758, 0.9992)static water

Role of St. Peter important at 2, 5 and 10



#### **Bold values are statistically significant results**

Table 1 Final model (95% confidence intervals in parentheses) 2 µg/L cutoff (n=283) 5 µg/L cutoff (n=283)  $10 \mu g/L cutoff (n=228)$ Variable (b<sub>i</sub>) Variable (b<sub>i</sub>) coefficient Variable (b<sub>i</sub>) coefficient coefficient Odds ratio Odds ratio Variable Type Odds ratio (multivariate) (multivariate) (multivariate) 0.8398 -0.3082 -0.3126 N/A N/A N/A N/A Intercept (0.3556, 1.4274)(-0.8791, 0.2581)(-0.8671, 0.3436)Distance to -0.3454 0.7079 -0.2553 0.7747 -0.2689 0.7642 nearest fold Continuous (-0.5215, -0.2254)(0.5936, 0.7982)(-0.4276, -0.1226) (0.6521, 0.8846)(-0.5821, -0.0900)(0.5587, 0.9139)Well open to St. 0.6532 1.9216 0.6805 1.9748 Peter Categorical N/A N/A (0.1197, 1.2225)(1.1271, 3.3956)(0.1910, 1.2400 (1.2104, 3.4555)Well open to -1.0684 0.3436 units below St. Categorical N/A N/A N/A N/A (-2 9185 -0 1396) (0.0540.0.8697) -0.0056 0.9945 -0.0058 0.9942 Continuous N/A N/A (-0.0092, -0.0026)(0.9908, 0.9974)(-0.0108, -0.0025)(0.9892, 0.9975)-0.0125 0.9876 N/A Continuous N/A N/A N/A (-0.0245, -0.0008)(0.9758, 0.9992)

Well construction also important. At 10 µg/L casing depth relative to the static water level becomes significant



#### **Bold values are statistically significant results**

Table 1         Final model (95% confidence intervals in parentheses)							
2 μg/L cutoff (			off (n=283)	5 μg/L cuto	ff (n=283)	10 μg/L cutoff (n=228)	
Variable	Variable Type	Variable (b <sub>i</sub> ) coefficient (multivariate)	Odds ratio	Variable (b <sub>i</sub> ) coefficient (multivariate)	Odds ratio	Variable (b <sub>i</sub> ) coefficient (multivariate)	Odds ratio
Intercept	N/A	<b>0.8398</b> (0.3556, 1.4274)	N/A	- <b>0.3082</b> (-0.8791, 0.2581)	N/A	- <b>0.3126</b> (-0.8671, 0.3436)	N/A
Distance to nearest fold axis	Continuous	<b>-0.3454</b> (-0.5215, -0.2254)	0.7079 (0.5936, 0.7982)	- <b>0.2553</b> (-0.4276, -0.1226)	0.7747 (0.6521, 0.8846)	- <b>0.2689</b> (-0.5821, -0.0900)	0.7642 (0.5587, 0.9139)
Well open to St. Peter Formation	Categorical	<b>0.6532</b> (0.1197, 1.2225)	1.9216 (1.1271, 3.3956)	<b>0.6805</b> (0.1910, 1.2400	1.9748 (1.2104, 3.4555)	N/A	N/A
Well open to units below St. Peter	Categorical	N/A	N/A	N/A	N/A	- <b>1.0684</b> (-2.9185, -0.1396)	0.3436 (0.0540, 0.8697)
Casing depth minus depth to bedrock	Continuous	<b>-0.0056</b> (-0.0092, -0.0026)	0.9945 (0.9908, 0.9974)	- <b>0.0058</b> (-0.0108, -0.0025)	0.9942 (0.9892, 0.9975)	N/A	N/A
Casing depth minus depth to static water level	Continuous	N/A	N/A	N/A	N/A	- <b>0.0125</b> (-0.0245, -0.0008)	0.9876 (0.9758, 0.9992)

$$L = b_0 + b_1 x_1 + b_2 x_2 \dots$$

Probability = 
$$\frac{e^L}{(1+e^L)}$$

Wisconsin Geological and Natural History Survey Division of Extension UNIVERSITY OF WISCONSIN-MADISON

Where x<sub>i</sub> are significant variables \_ from the previous slide \_

Variables known for 3200 wells in the two counties



$$L = b_0 + b_1 x_1 + b_2 x_2 \dots$$

Probability = 
$$\frac{e^L}{(1+e^L)}$$



Where x<sub>i</sub> are significant variables from the previous slide Variables known for 3200 wells in the two counties



	Bulk average - No regulations	
Probability ≥2 μg/L	56.7%	
Probability ≥5 μg/L	35.4%	
Probability ≥ 10 μg/L	20.3%	





## Summary

- Wells drilled near folds (faults?) have a higher probability of detecting arsenic, perhaps due to more sulfide or arsenic-bearing hydroxides
- Wells drilled in the St. Peter Formation have a higher probability of detecting arsenic
- It is best for groundwater wells to case far below the bedrock surface and the static water level
- The amount of arsenic contained in sulfide minerals decreases below the sulfide cement horizon, making the stratigraphically lower units safer
- Combining 3D geologic mapping with logistic regression allows us to predict risk as well as the impact of casing regulations, which could reduce, but not eliminate arsenic risk, particularly at higher concentrations